



Solid oxide fuel cell combined heat and power: Future-ready Energy



# SmartCHP final conference Cogenerating a renewable future

## The role of small-scale bio- CHP in Europe's Energy mix

### BLAZE & SO-FREE projects



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The JU receives support from the European Union's Horizon 2020 research and innovation programme and Italy, Austria, Finland, Germany, Poland, Netherlands, United Kingdom

## CHP IN EU-28 (Eurostat)

- 120 GWe (ST 50%, CC 25%, ICE 13%, GT 10%): 362 TWh -> ≈3000 AEh (≈ 11% of electricity demand).
- 300 GW<sub>th</sub>: 775 TWh -> ≈ 2500 AEh
- space heating ≈ 50% process heating (Germany, Italy, Poland and the Netherlands largest capacity)
- Natural gas ≈ 50%, solid fossil fuels and peat ≈ 20% , oil and oil products 5%, biomass (timber by-products, black liquor, wood, straw, animal waste, OFMSW) attained 20% but there is difficulty in converting different biomass feedstocks in a Reliable and Economic (Efficient and Clean) way
- Zero Energy Buildings (ZEB&ZED) from 31st December 2020 (public buildings from 31<sup>st</sup> December 2018)



## CHP SoA & BLAZE foreseen goals

Below 1 MWe systems mainly applied :

1. Biomass combustor coupled to organic rankine cycle (ORC)
2. Biomass fixed bed gasifier coupled to internal combustion engine (ICE)

BLAZE 100 (100 kWth biomass DBFBG integrated with 50 kWe SOFC) is compared to a 100 kWth biomass combustor coupled to a 15 kWe ORC and a 100 kWth biomass fixed bed gasifier coupled to a 25 kWe ICE

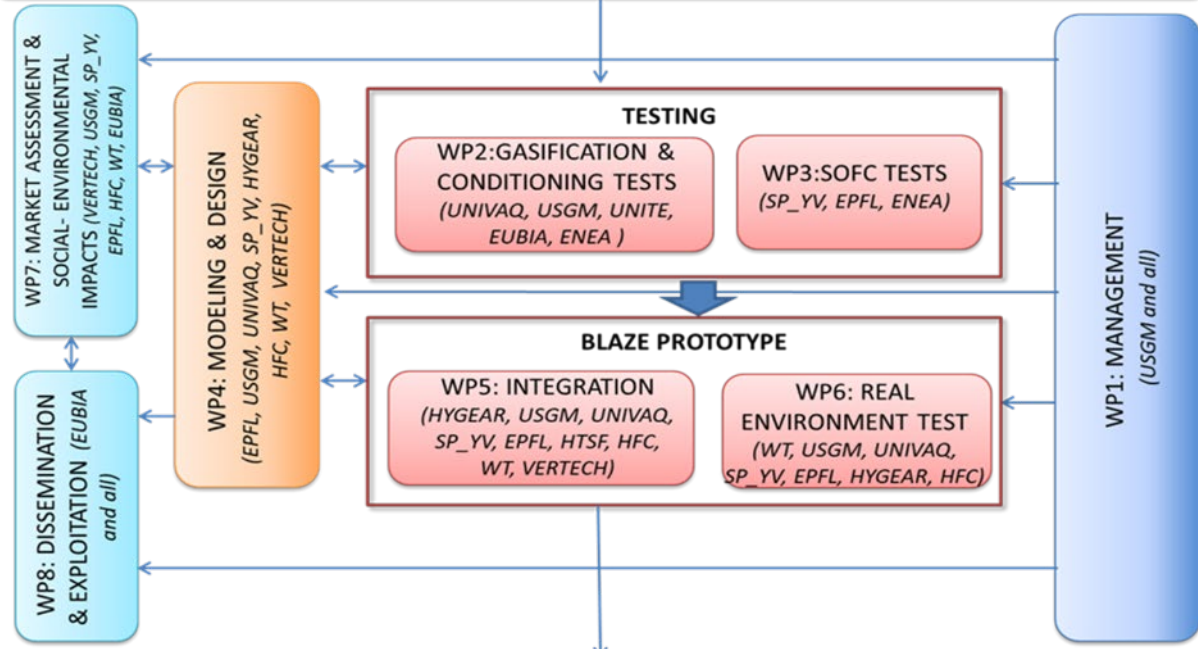
Cost of a gas boiler with burner, flue tubes and accessories is added to the CHP plants cost. To this item, heating civil works, piping, pump, expansion vessel and regulation system have been added.

Buildings heat price: 0.06 €/kWht (AEH: 3000 electrical and 2500 thermal) Industrial heat price: 0.04 €/kWht (AEH: 7500 electrical and thermal).

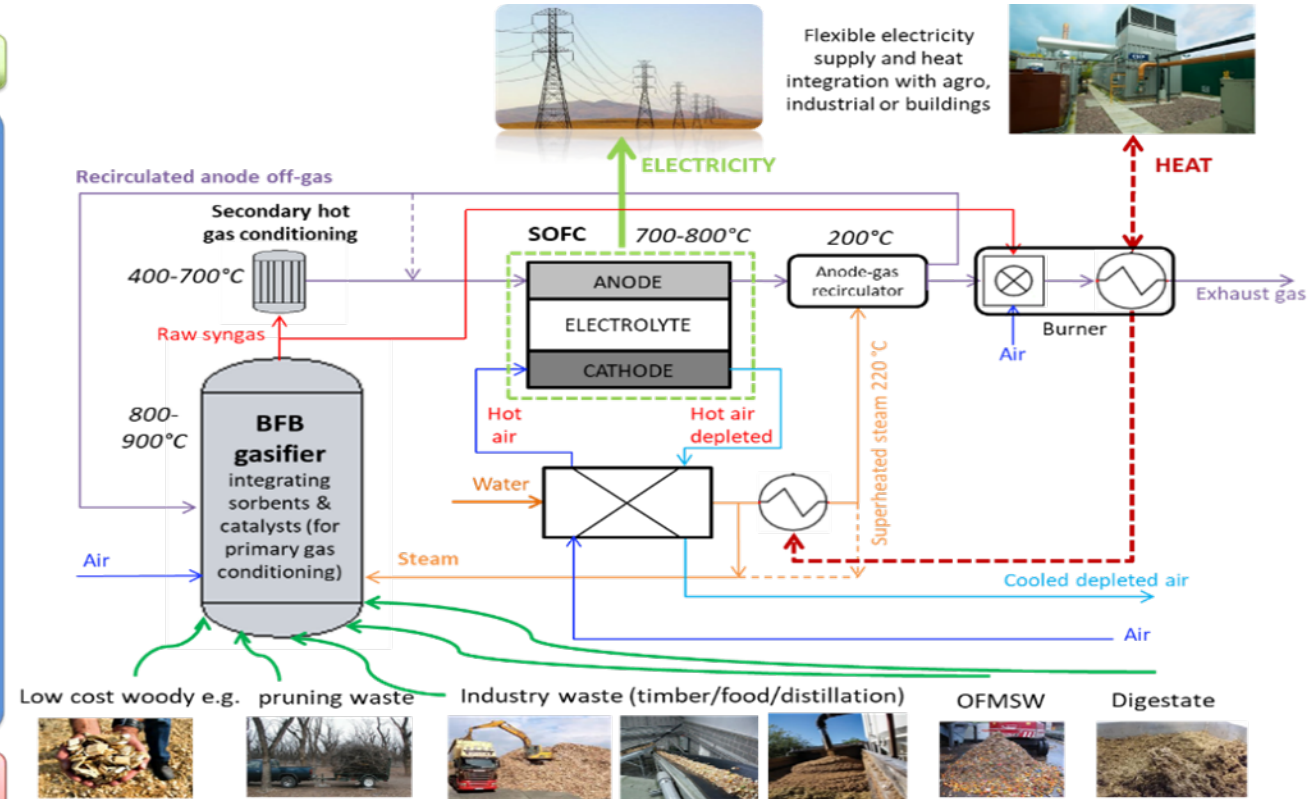
Biomass price: 60 €/ton (similar to the price of high humidity wood chips for BLAZE) 100 €/ton (similar to the price of low humidity wood chips for ORC and ICE systems).

BLAZE: overall 90% (versus 65%, target SET-PLAN 75%), electrical 50% (versus 25%, target SET-PLAN >30%), near-zero gaseous and PM emissions, CAPEX below 4,000 €/kWe (actual 10,000 €/kWe), OPEX of ≈ 0.05 €/kWhe (actual 0.10 €/kWhe), electricity production cost 0.10 €/kWh (actual 0.22 €/kWh, SET-PLAN target of 20% cost reduction by 2020, and 50% by 2030).

Objectives: to develop Biomass, Low cost, Advanced and Zero Emission small-medium scale CHP plant «BLAZE»



Results: Breakthrough in the cost reduction and performance increase of biomass small and medium CHP



## Research Partners

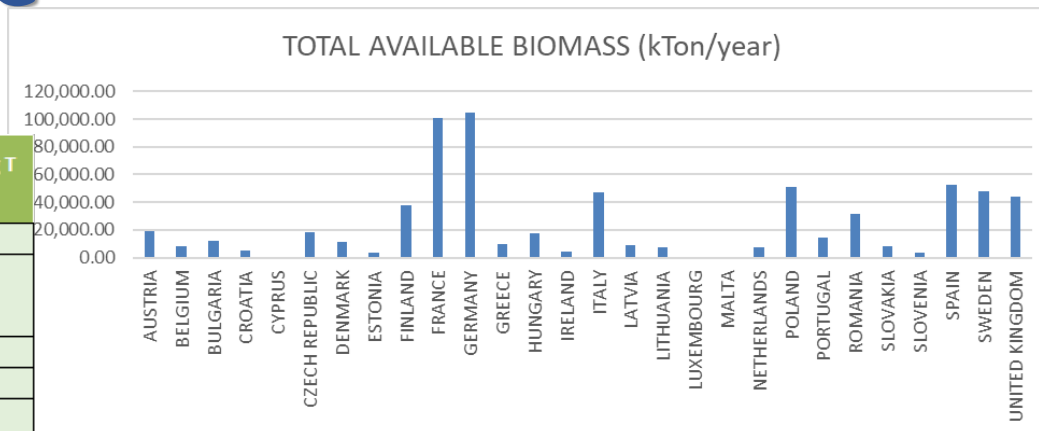


## Companies Partners



## N.P. Partners





Feedstock	CATEGORY	Humidity (%-wt, as received)	LHV MJ/kg	Ash %wt, dry basis	S %wt, dry basis	Cl %wt, dry basis	Ash melting T (DT) (°C)
Subcoal	Municipal waste	3,20	21,68	15,60	0,10	1,00	1250,00
Olive pomace pitted	Secondary residues of industry utilising agricultural products	36,30	19,79	5,95	0,06	0,08	1290,00
Sawmill waste	Primary residues from forest	11,20	18,89	0,41	<0.01	<0.01	1300,00
Multi-essence wood chips	Waste from wood	24,50	17,88	1,45	0,02	<0,01	1370,00
Olive Prunings	Secondary residues from wood industries	14,90	17,76	1,55	<0.01	<0.01	1380,00
Almond shells	Secondary residues of industry utilising agricultural products	10,00	17,68	1,31	<0.01	<0.01	1000,00
Swarf and sawdust	Secondary residues from wood industries	6,60	17,14	0,43	<0.01	<0.01	>1385
Wood chips	Primary residues from forest	8,90	16,74	0,54	<0.01	<0.01	>1385
Corn cobs	Agricultural residues	9,00	16,62	3,04	0,03	0,44	645,00
Arundo Donax	Agricultural residues	10,10	16,25	3,43	0,11	0,29	1185,00
1- Wheat Straw (pellets 10 mm)	Agricultural residues	7,60	15,98	9,22	0,05	0,12	1065,00
2- Wheat Straw (pellets 6 mm)	Agricultural residues	7,60	15,40	13,29	0,08	0,21	1135,00
Rice husks	Secondary residues of industry utilising agricultural products	5,20	15,19	14,70	0,02	0,03	990,00
Digestate	Digestate from biogas production	71,20	12,69	25,81	0,97	0,10	1245,00
Black Liquor	Secondary residues from wood industries	20,60	11,20	48,28	0,74	0,12	680,00
Municipal solid waste	Municipal waste	23,00	10,22	47,01	0,20	0,40	1220,00

CATEGORY	potential (Kton dry mass/y)
Agricultural residues	264986,32
Primary residues from forest	167641,91
Municipal waste	89763,53
Secondary residues from wood industries	87906,47
Secondary residues of industry utilising agricultural products	29527,11
Waste from wood	26418,22
Digestate from biogas production	12634,60

CATEGORY	cost €/ton
Waste from wood	15
Agricultural residues	28
Primary residues from forest	35
Secondary residues from wood industries	35
Secondary residues of industry utilising agricultural products	55
Municipal waste	60
Digestate from biogas production	661



Olive pomace



Almond shells

Feedstock	%wt, dry basis					
	C	H	N	S	Cl	O
OP	51.8	7.1	2.8	0.06	0.08	32.1
AS	48.8	6.1	0.5	< 0.01	< 0.01	43.2



Calcined Dolomite



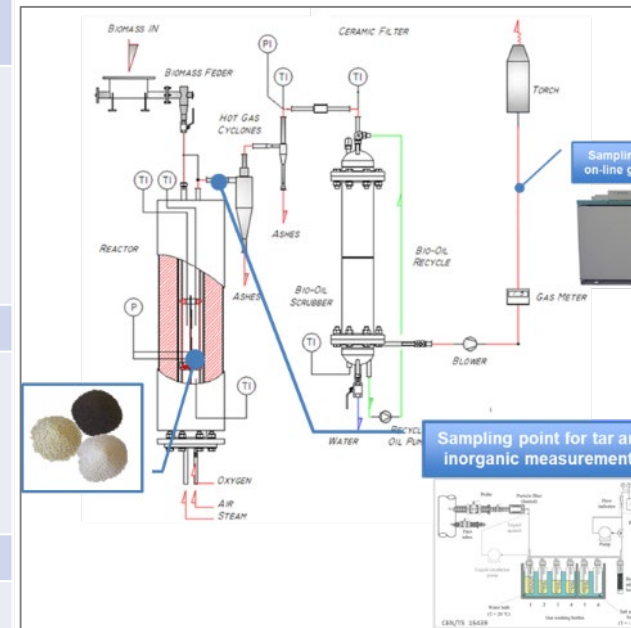
Na<sub>2</sub>CO<sub>3</sub>

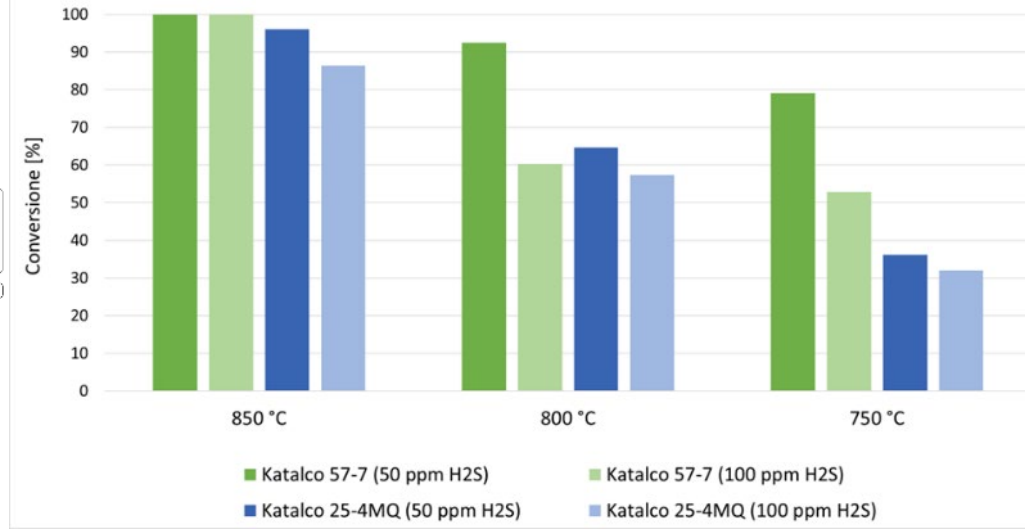
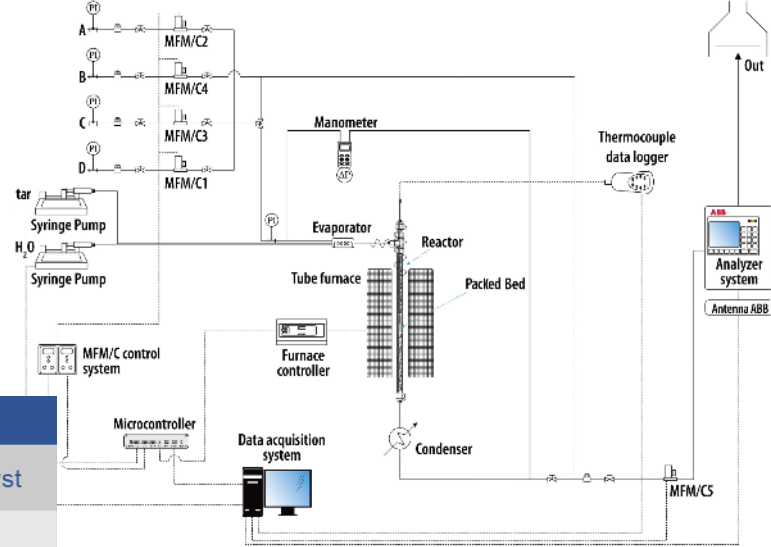


K<sub>2</sub>CO<sub>3</sub>

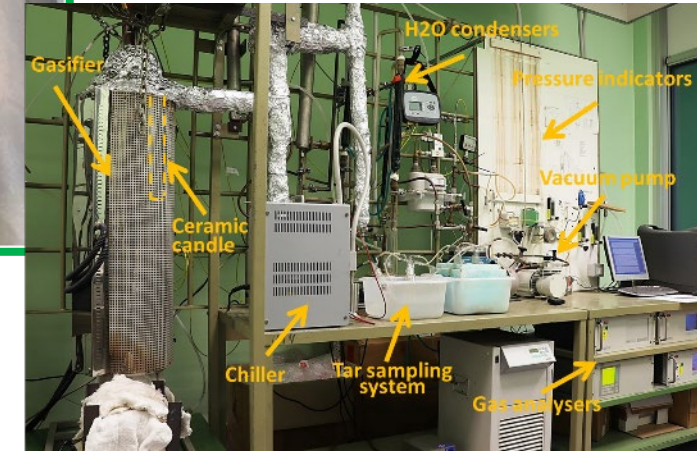
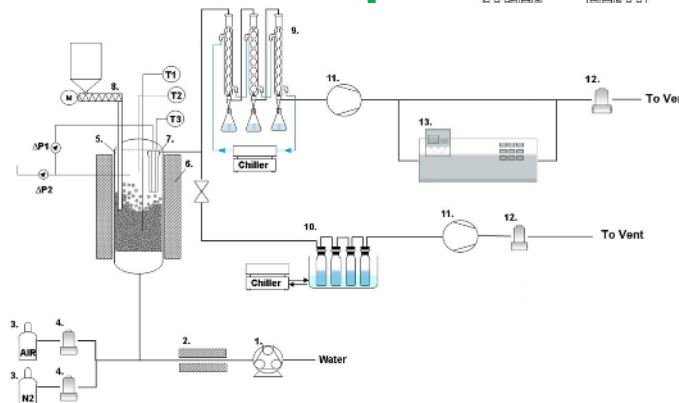
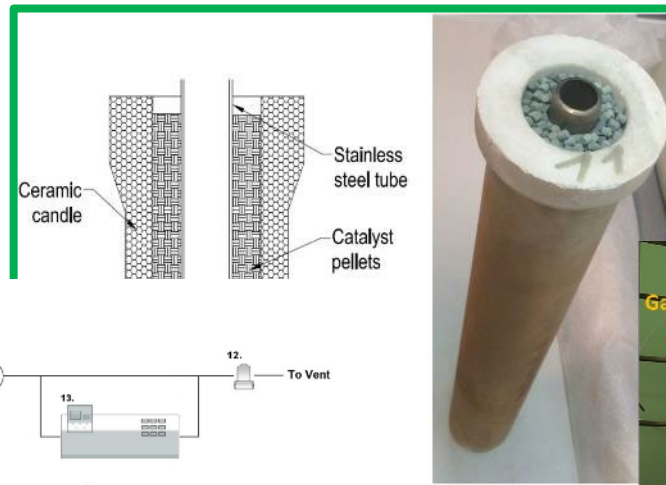
- Bed material (i.e. olivine, calcined dolomite)
- In-bed sorbents (i.e. calcined dolomite, Na<sub>2</sub>CO<sub>3</sub>, K<sub>2</sub>CO<sub>3</sub>)

In-bed implementation	Observed Effect	
	Olive Pomace	Almond shells
Primary additives		
Na <sub>2</sub> CO <sub>3</sub> , K <sub>2</sub> CO <sub>3</sub> : x 100 stoich.	1- Reduction of HCl content around ≈ 10-100 mg/Nm <sup>3</sup> <sub>dry</sub> vs 510 mg/Nm <sup>3</sup> <sub>dry</sub> (theoretical value).	1- Reduction of HCl content < 20 mg/Nm <sup>3</sup> <sub>dry</sub> vs 55 mg/Nm <sup>3</sup> <sub>dry</sub> (theoretical value)
c-Dolomite (0-45 %-wt)	1- Appreciable effect on gas composition (H <sub>2</sub> enrichment, from 25 %-v up to 35 %-v, N <sub>2</sub> -free); 2- Important effect on Tar content reduction (%-eff: > 45%-wt on Tot GCMS: 25 g/Nm <sup>3</sup> <sub>dry</sub> vs 13.7 g/Nm <sup>3</sup> <sub>dry</sub> ; Benzene, Toluene, Naphthalene ≈ 1000s mg/Nm <sup>3</sup> <sub>dry</sub> ); 3- H <sub>2</sub> S content reduced to tens/few mg/Nm <sup>3</sup> <sub>dry</sub> (vs 320 mg/Nm <sup>3</sup> <sub>dry</sub> (theoretical value));	1- No appreciable effect on gas composition (H <sub>2</sub> content ~ 35 %-v, N <sub>2</sub> -free); 2- Important effect on Tar content reduction (%-eff: > 50%-wt on Tot GCMS: 28 g/Nm <sup>3</sup> <sub>dry</sub> vs 10 g/Nm <sup>3</sup> <sub>dry</sub> ; Benzene, Toluene, Naphthalene ≈ 1000s mg/Nm <sup>3</sup> <sub>dry</sub> ); 3- H <sub>2</sub> S content reduced to tens/few mg/Nm <sup>3</sup> <sub>dry</sub> vs 27 mg/Nm <sup>3</sup> <sub>dry</sub> (theoretical value);
Steam/Biomass (OLV)		
0.5 vs 1.0	1- H <sub>2</sub> enrichment (H <sub>2</sub> : 25 → 35 %-v, N <sub>2</sub> -free basis); 2- limited reduction on light hydroc. content (i.e. CH <sub>4</sub> + C <sub>2</sub> H <sub>x</sub> ); 3- lower effect on the reduction of tar content 25 g/Nm <sup>3</sup> <sub>dry</sub> (~ 30% based on Tot GCMS);	1- H <sub>2</sub> enrichment (H <sub>2</sub> : 35 → 45 %, N <sub>2</sub> -free basis); 2- No effect evidence on light hydroc. content (i.e. CH <sub>4</sub> + C <sub>2</sub> H <sub>x</sub> ); 3- lower effect on the reduction of tar content 28 g/Nm <sup>3</sup> <sub>dry</sub> vs 19 g/Nm <sup>3</sup> <sub>dry</sub> (~ 30% based on Tot GCMS);
Equivalence Ratio		
0.25 vs 0.30	1- Minimal effect on gas composition (CO <sub>2</sub> %-v increase); 2- Limited effect in the tar content (~ 15-20%-wt on Tot GCMS);	1- Minimal effect on gas composition (CO <sub>2</sub> %-v increase); 2- Limited effect in the tar content (~ 15%-wt on Tot GCMS);



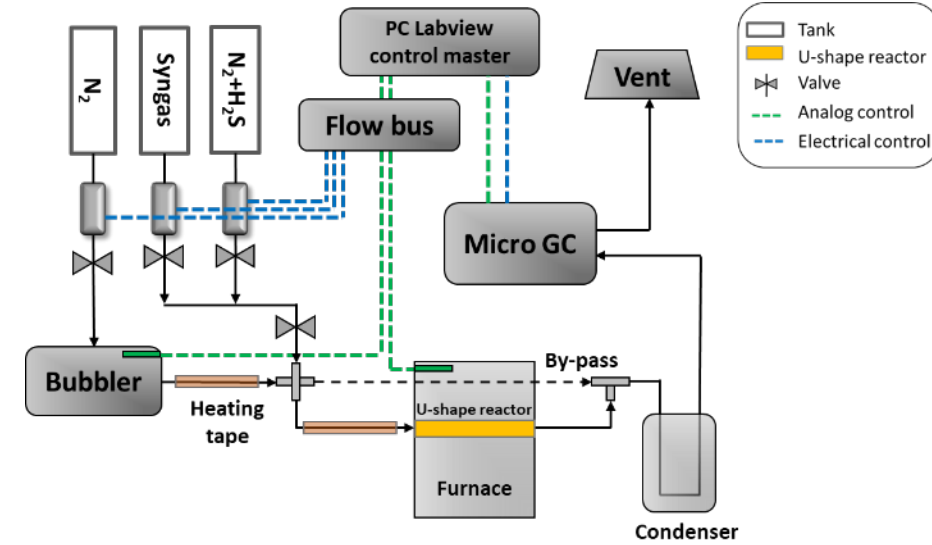


Test	#8	#10	#11
Ceramic candle	Partially filled catalyst B	Olivine + dolomite	2x Catalyst
Bed material	Olivine	Olivine + dolomite	
Avg Temperature (°C)	848	844	844
Steam/Biomass	0.52	0.50	0.58
GHSV (h <sup>-1</sup> )	4492	4227	2324
Gas yield (Nm <sup>3</sup> dryN <sub>2</sub> free/kg <sub>bio</sub> )	1.84	1.87	1.89
H <sub>2</sub> O conversion (%)	56.24	54.84	58.24
H <sub>2</sub> (%vol dryN <sub>2</sub> free)	55.69	55.06	53.31
CO (%vol dryN <sub>2</sub> free)	31.59	31.39	34.73
CO <sub>2</sub> (%vol dryN <sub>2</sub> free)	11.05	12.12	11.34
CH <sub>4</sub> (%vol dryN <sub>2</sub> free)	1.67	1.44	0.61
LHV (MJ/Nm <sup>3</sup> )	9.04	8.85	8.75
H <sub>2</sub> (NI/min)	10.10	10.17	10.24
Toluene/1-ring (mg/Nm <sup>3</sup> dryN <sub>2</sub> free)	73/46	N.D./389	N.D./208
Naphthalene/2-ring (mg/Nm <sup>3</sup> dryN <sub>2</sub> free)	162	85	N.D.
Total Tar (w/o benz) (mg/Nm <sup>3</sup> dryN <sub>2</sub> free)	342	474	208



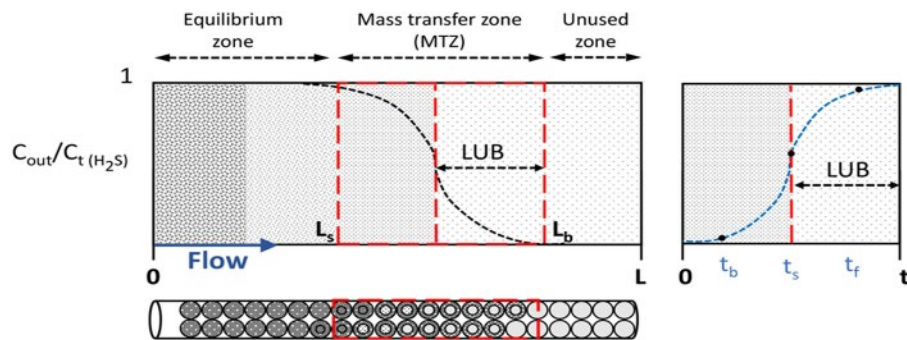


Paper published in Energies journal : E. Ciro, A. Dell’Era, A. Hatunoglu, L. Del Zotto, E. Bocci  
*Kinetic and Thermodynamic Study of the Wet Desulfurization Reaction of ZnO Sorbents at High Temperatures*



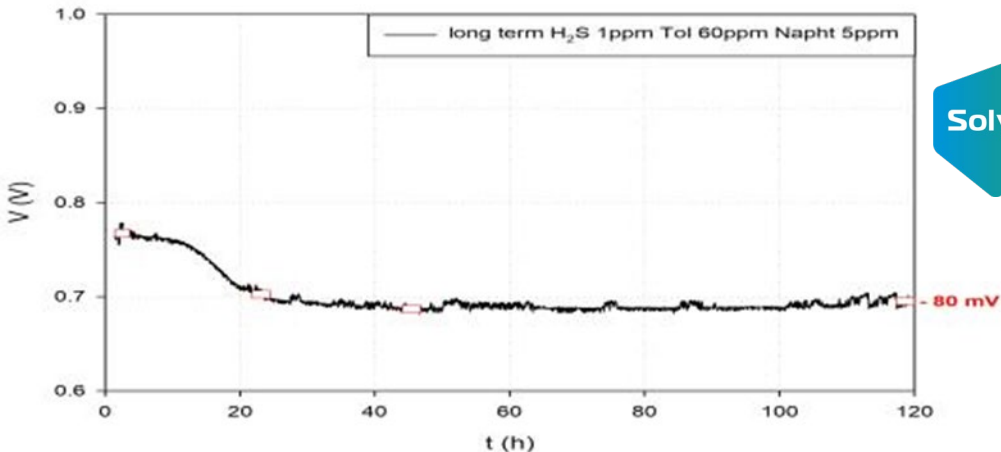
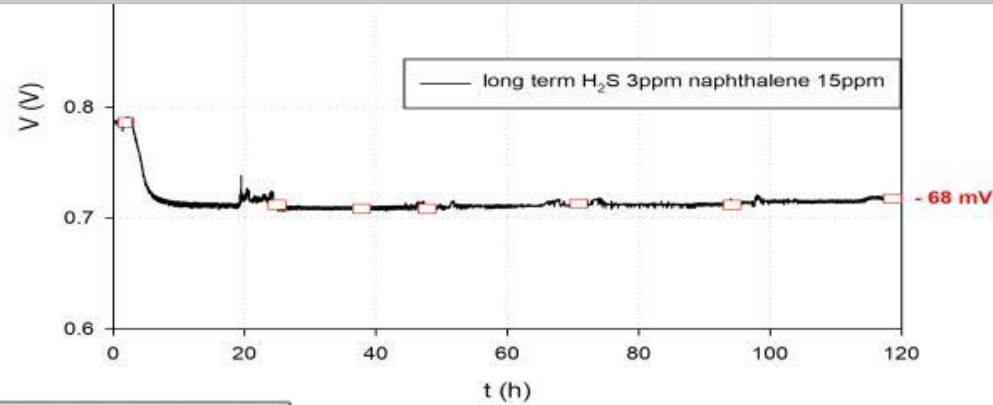
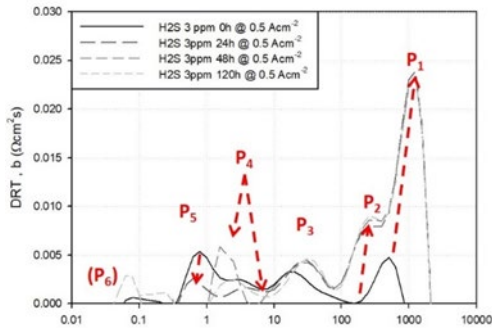
- ZnO sorbents showed the best performances of absorption capacity of the at 550 °C, achieving a sorption capacity of 5.4 g per 100 g of sorbent and a breakthrough time of 2.7 h.
- These materials also have been shown acceptable results up to 600 °C.
- A water-gas shift (WGS) and a catalytic reactions was observed on the ZnO performance.
- From thermodynamic analysis, the endothermic features for the deactivation reaction was observed and thermodynamic calculations for enthalpy, entropy, activation energy and diffusion coefficient were calculated.
- The modelling of the bed fixed reactor and subsequent estimations of bed reactor were carried out to sizing the dimensions of a fixed bed reactor.

Experimental Conditions	I	II
Gas flow	<b>Syngas*</b>	
Sorbent (g)	0.5–0.25	
T (°C)	450–600	
P (bar)	0.95–1.05	
GHSV (10 <sup>3</sup> h <sup>-1</sup> )	25–50	
C <sub>H<sub>2</sub>S</sub> (ppmv)	400	260
BL (cm)	0.8–1.5	
Bed L/D index	1–1.9	
Particle size (mm)	1.5–3.0	
Total flow (NmL min <sup>-1</sup> )	305 ± 1	

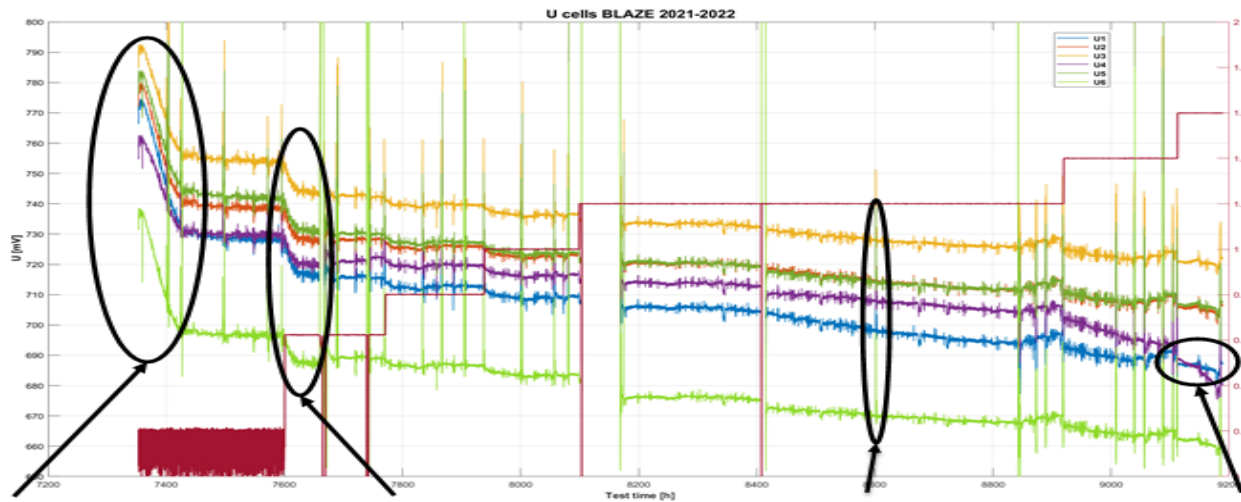




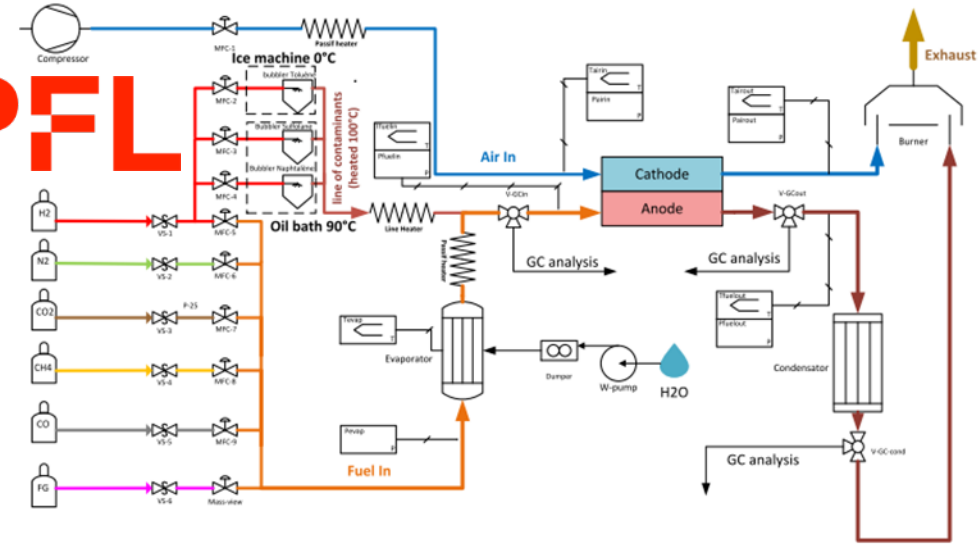
Contaminant thresholds	H <sub>2</sub> S		1-ring tar Toluene		2-ring tar Naphthalene	
	Low	High	Low	High	Low	High
ppm(v)	1	3	60	180	5	15
mg/Nm3 (dry)	-	-	250	750	25	85



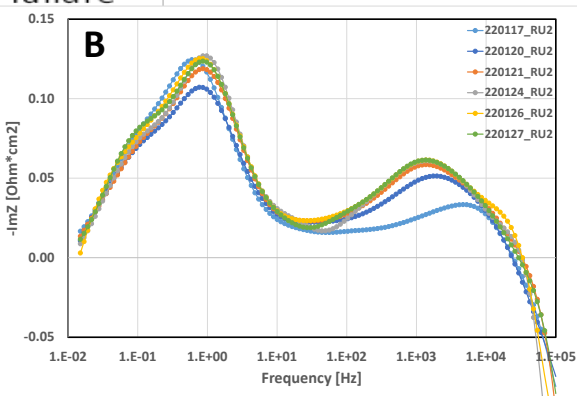
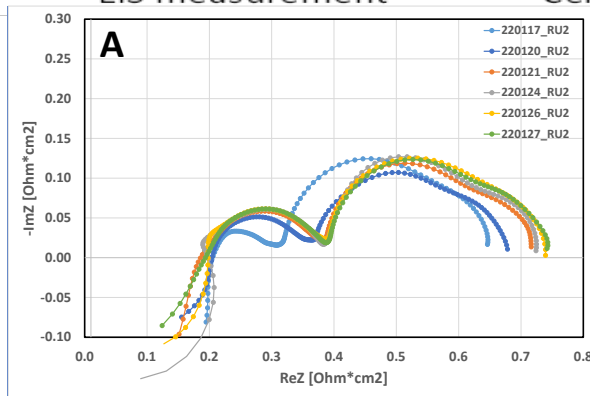
- Several tests were performed to analyse single and multi-contaminant impact on syngas-fed SOFC
- The multi-contaminant tests generally confirm the results obtained from the single-contaminant (H<sub>2</sub>S mainly affecting charge transfer; tars affecting R0 and diffusion but also charge transfer)
- R0 mobility was observed for the tar-laden syngas compositions, possibly due to C-dep which induces a dynamic effect on R0
- Tar presence (in smaller concentrations and with cells with higher initial voltage) seem to mitigate the H<sub>2</sub>S poisoning (possibly due to a concomitant activity of Ni for tar reforming). This is however not observed for all samples, being related to H<sub>2</sub>S/Tar ratio and Tar typology



EPFL

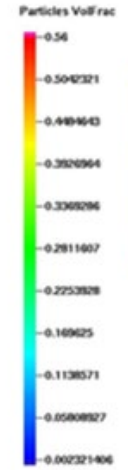
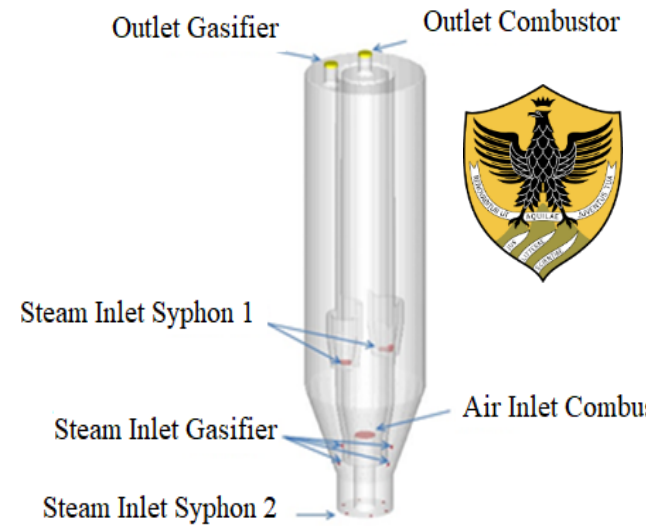
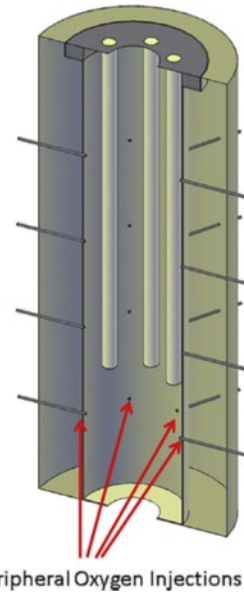
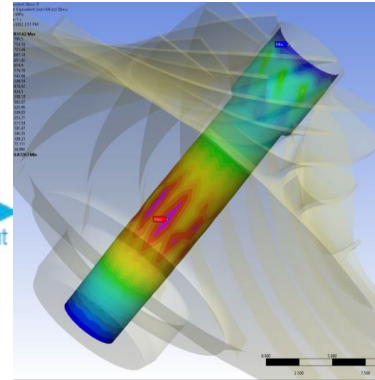
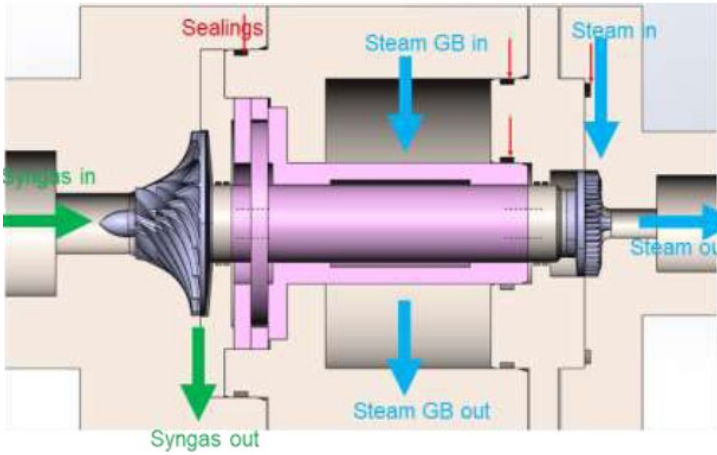


Initial drop, under 2ppm H<sub>2</sub>S      Second drop, under 0.625ppm H<sub>2</sub>S

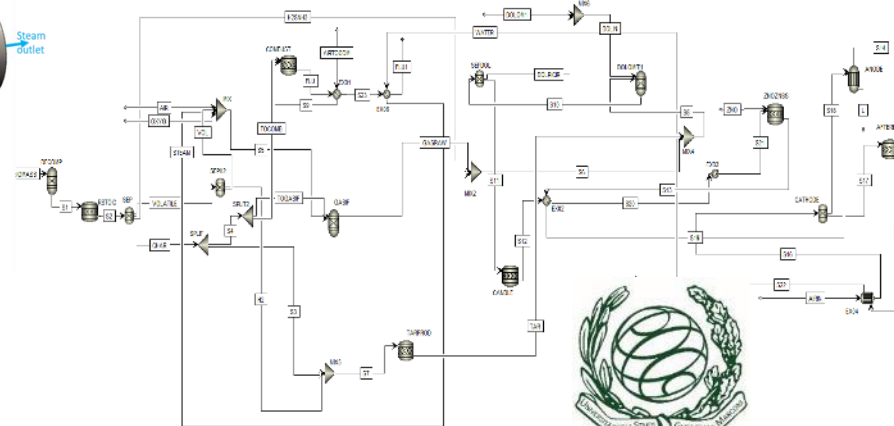
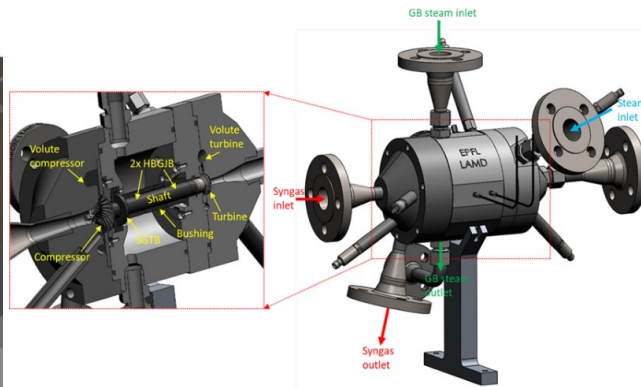
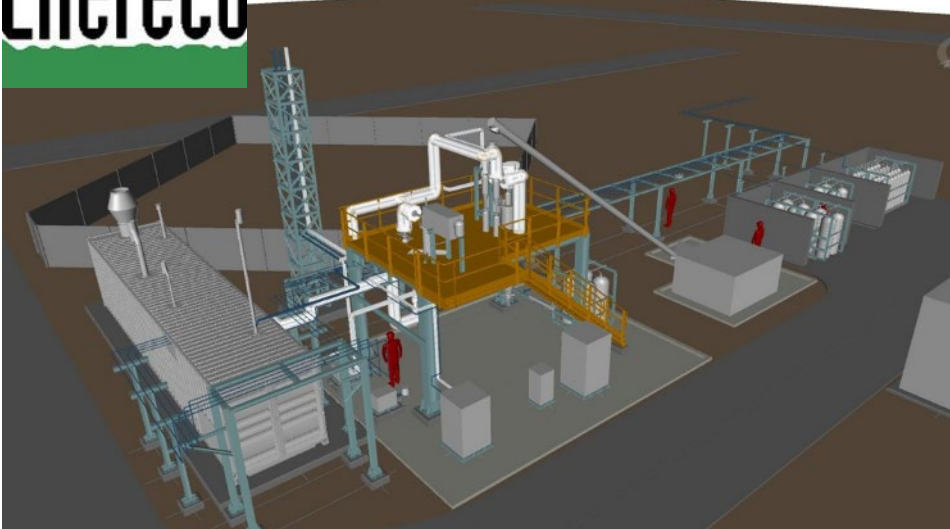


- 3 short stacks tested 22'500h in total
- 3700h of impurities exposure Sulfur (DMS): 0.2 → 4ppm Light tar (Toluene): 20 → 400ppm Halogen (HCl): 5 → 50ppm
- EIS under nominal polarization DRT analysis
- stable operation in clean syngas (9000h) -3.4 μV/h (-0.4%/kh)
- S deactivates Ni starting from 0.2ppm (30ppb) Affects CT and RWGS 9% voltage drop at 4ppm Co-feed of toluene mitigates S-contamination Partial recovery (logarithmic) 50% in 33h 80% in 250h
- HCl leads to irreversible degradation (-60 μV/h) for 5-50ppm

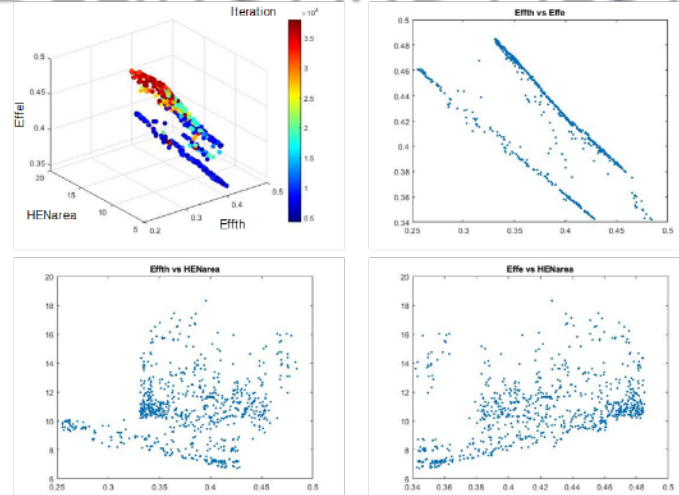
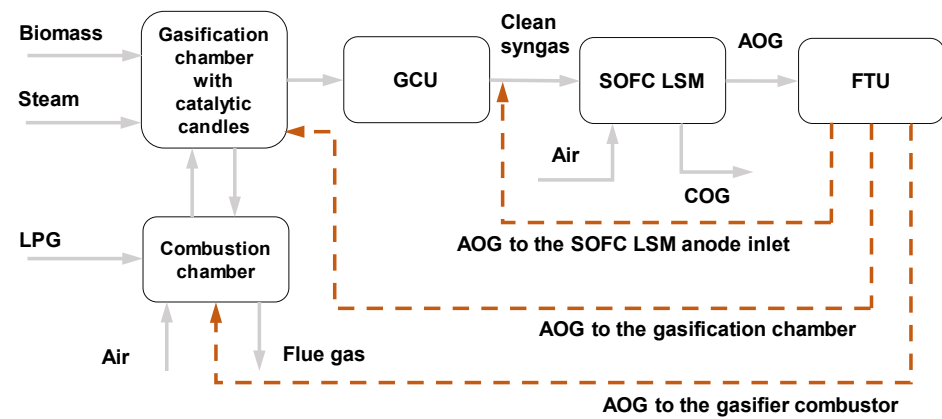
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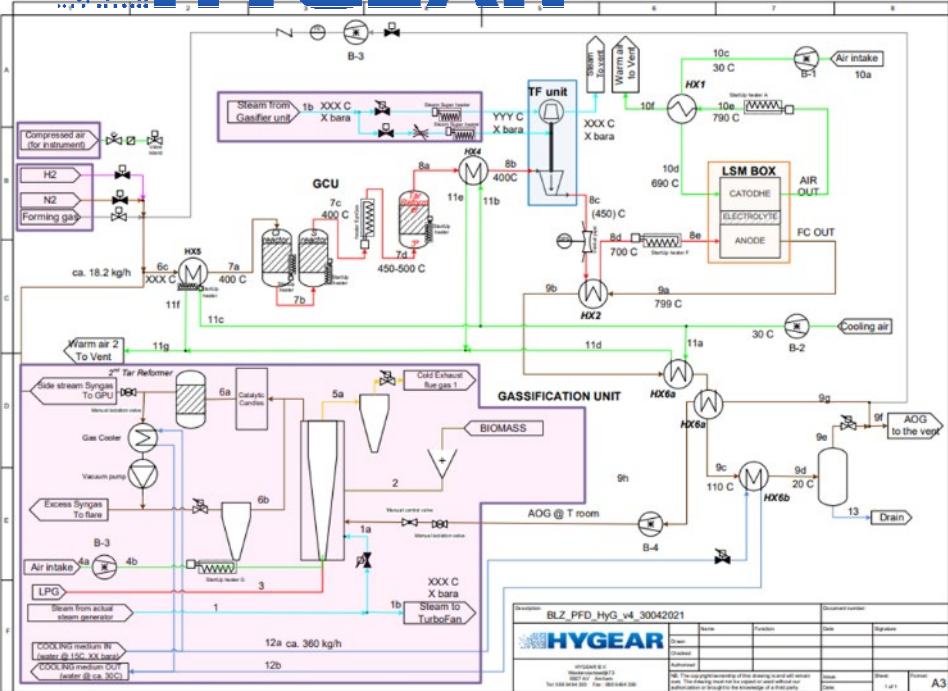
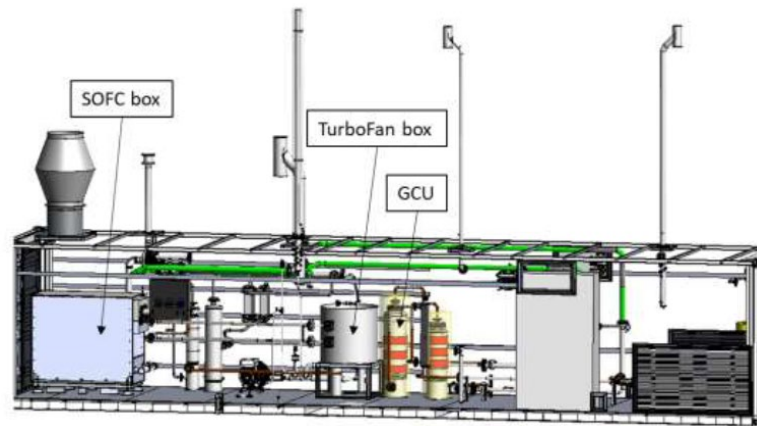
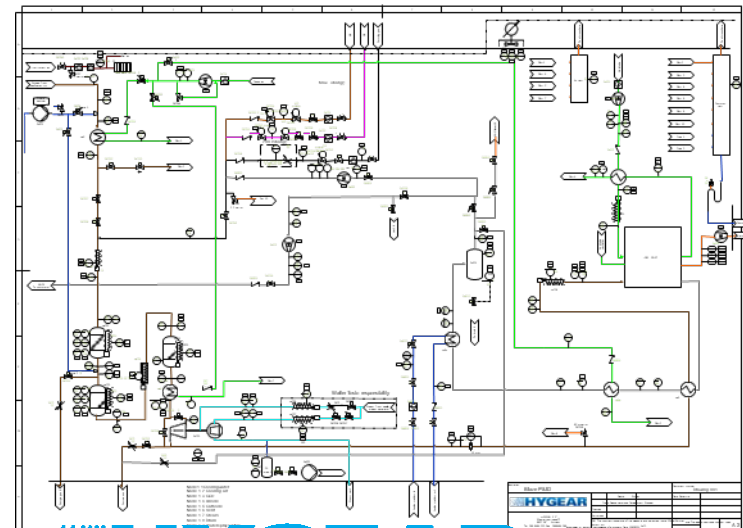
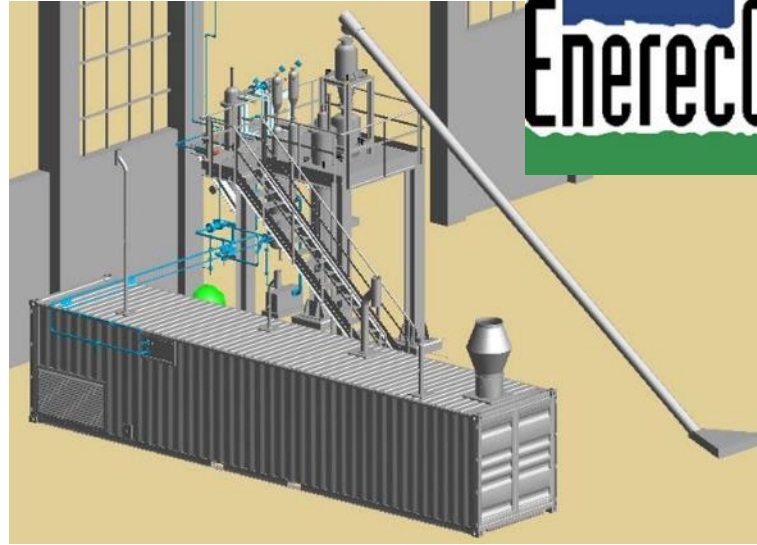
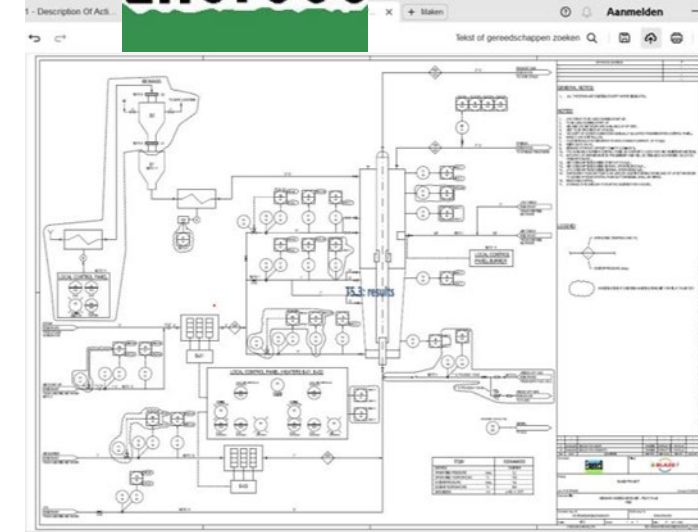


Name	Description
Case 1	Base case; BLAZE plant without AOG use.
Case 2	AOG recirculation to the gasification chamber.
Case 3	AOG recirculation to the SOFC LSM anode inlet.
Case 4	AOG recirculation to the gasifier combustor without FTU.
Case 5	AOG recirculation to the gasifier combustor with FTU.
Case 6	AOG used in a GT.

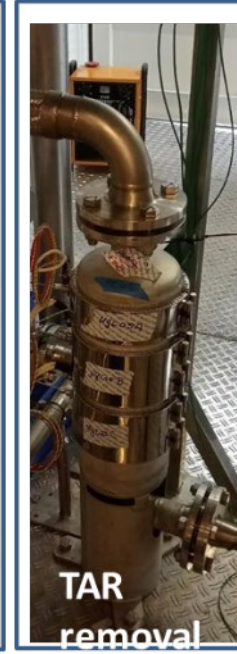
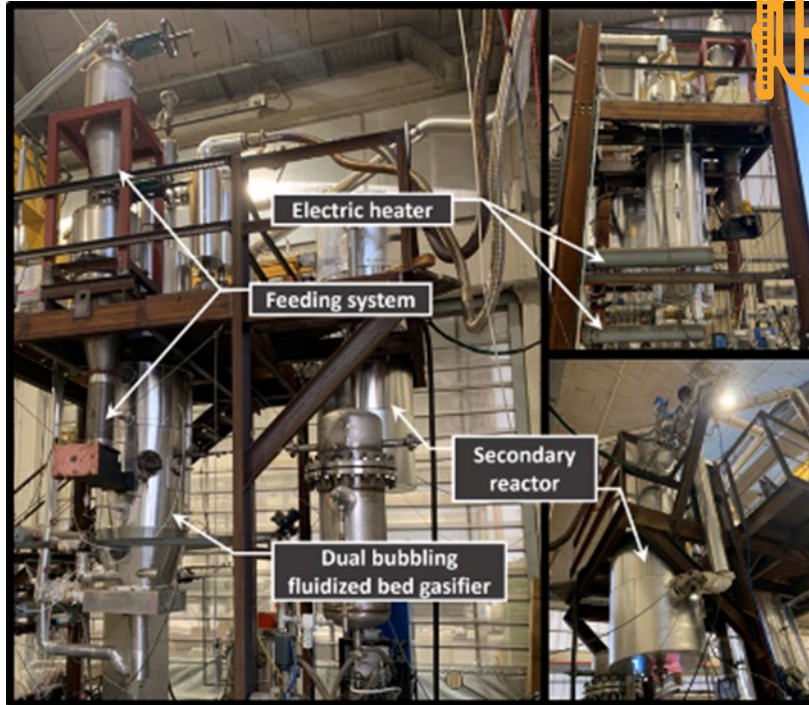
	Case 1	Case 2	Case 3	Case 4	Case 5	Case 6
Gross power SOFC (kW)	25	25	25	25	25	25
Gross power turbine (kW)						8.973
Air compressor (gasifier) (kW)	0.291	0.363	0.316	0.327	0.226	0.292
Air compressor (SOFC) (kW)	0.663	0.746	0.611	0.663	0.663	0.663
AOG compressor (kW)	0	0.098	0.123	0.129	0	1.361 <sup>1</sup>
Pumps (kW) <sup>2</sup>	6.00E-05	3.24E-03	6.12E-04	6.00E-05	6.00E-05	1.00E-03
Net power (kW)	24.046	23.788	23.947	23.877	24.106	31.656
CGE	0.73	0.75	0.68	0.68	0.75	0.73
SOFC efficiency	0.50	0.47	0.50	0.50	0.50	0.50
Eff <sub>el</sub>	0.34	0.37	0.39	0.38	0.44	0.45
Cooling water produced (kg/h)	189.68	213.61	174.52	189.68	189.68	189.68
Cooling water produced (kW)	9.51	10.72	8.75	9.51	9.51	9.51
Cold utility (kW)	6.23	8.06	18.75	18.35	4.72	17.41
Eff <sub>th</sub>	0.22	0.28	0.45	0.45	0.25	0.38
Total efficiency (Eff <sub>el</sub> + Eff <sub>th</sub> )	0.57	0.65	0.83	0.83	0.69	0.84
<b>FTU</b>						
ΔP (mbar)		250	60		270	
Steam needed (kg/h)		19.85	3.75		10.19/16.50	
Inlet fan T (°C)		200	200		20/200	
Total power needed from turbine (kW)		0.315	0.060		0.162/0.209	

Variable / criterion	Distance utopian	Eff <sub>el</sub>	Eff <sub>th</sub>	HEN area
FU	0.780	0.800	0.715	0.746
STB	0.333	0.330	0.967	0.330
T <sub>gasif</sub> (°C)	782.475	751.173	837.502	839.452
T <sub>inSOFC</sub> (°C)	690.000	690.391	697.473	690.022
TC2 (°C)	28.705	25.873	26.207	186.869
TH1 (°C)	550.054	745.798	132.408	101.537
TH6S (°C)	321.274	398.596	356.899	221.770
TC1 (°C)	279.412	200.000	236.054	428.615
TH2 (°C)	642.955	550.967	634.334	626.737
TH3 (°C)	508.714	756.581	245.333	263.241
Eff <sub>el</sub>	0.4547	0.4873	0.3443	0.3493
Eff <sub>th</sub> *	0.3558	0.3052	0.4736	0.4093
Eff <sub>tot</sub>	0.8105	0.7925	0.8179	0.7587
Area (m <sup>2</sup> )	9.980	11.543	13.614	6.727
Steam generated (kg/h)	14.606	10.027	29.977	26.360
Cooling water produced (kg/h)	155.826	153.954	190.537	161.233
Steam to gasifier (kg/h)	3.261	3.158	10.696	3.371
LPG (kg/h)	0.173	0.000	0.902	1.196
Recirculation compressor (kW) @ TC2	0.122	0.115	0.153	0.360
Steam needed in the FTU (kg/h) @ TC2	9.63	9.13	12.10	28.05
Steam needed in the FTU (kg/h) @ 200 °C	15.11	14.35	19.05	1

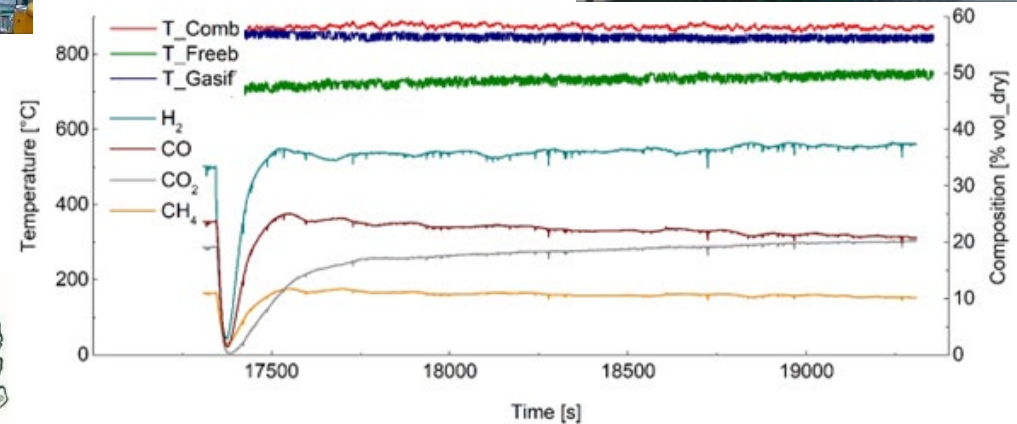
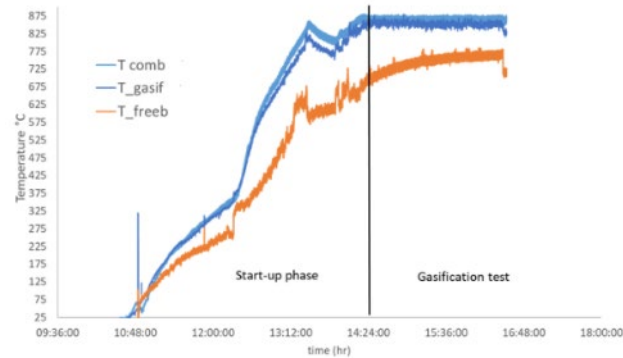
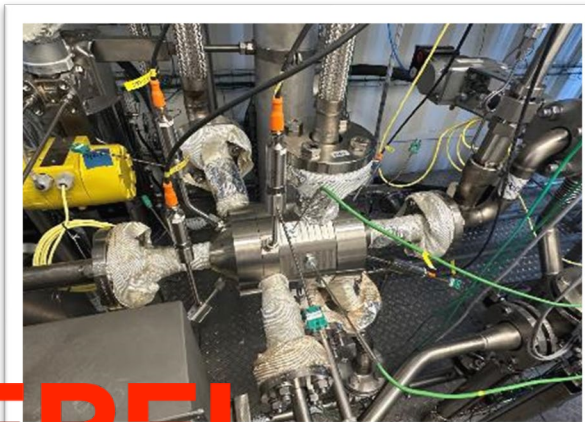
## Overall CHP pilot system: Gasification unit + CHP sub-units

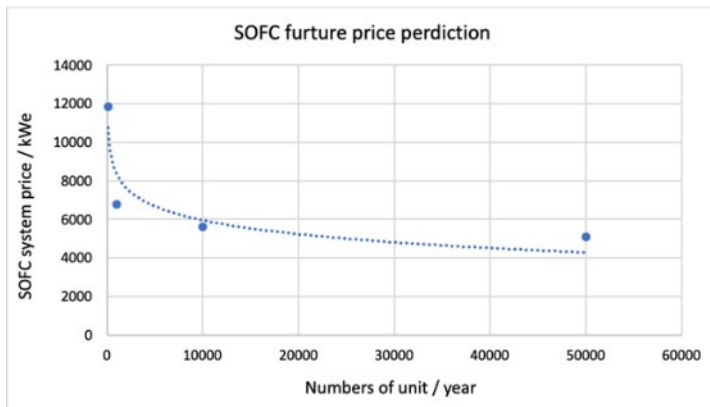
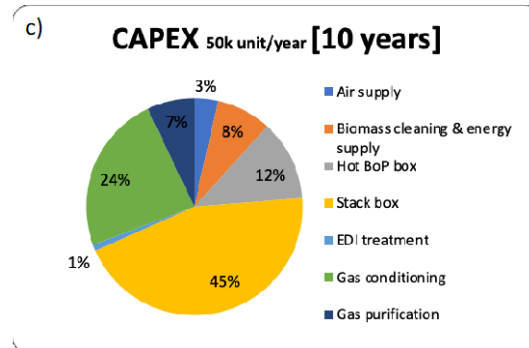
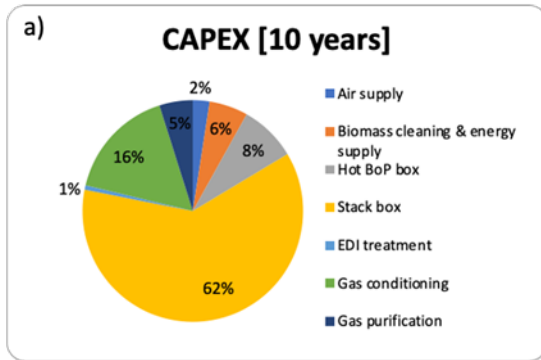


- Double Bubbling Gasifier/Combustor
  - Gas cleaning unit (GCU)
  - Turbo-fan/steam driven compressor (TF)
  - 25 kWe Large Stack Module (LSM)
  - Anode off gas post-processing section
- BoP, PID, HAZID, HAZOP done!



SolydEra

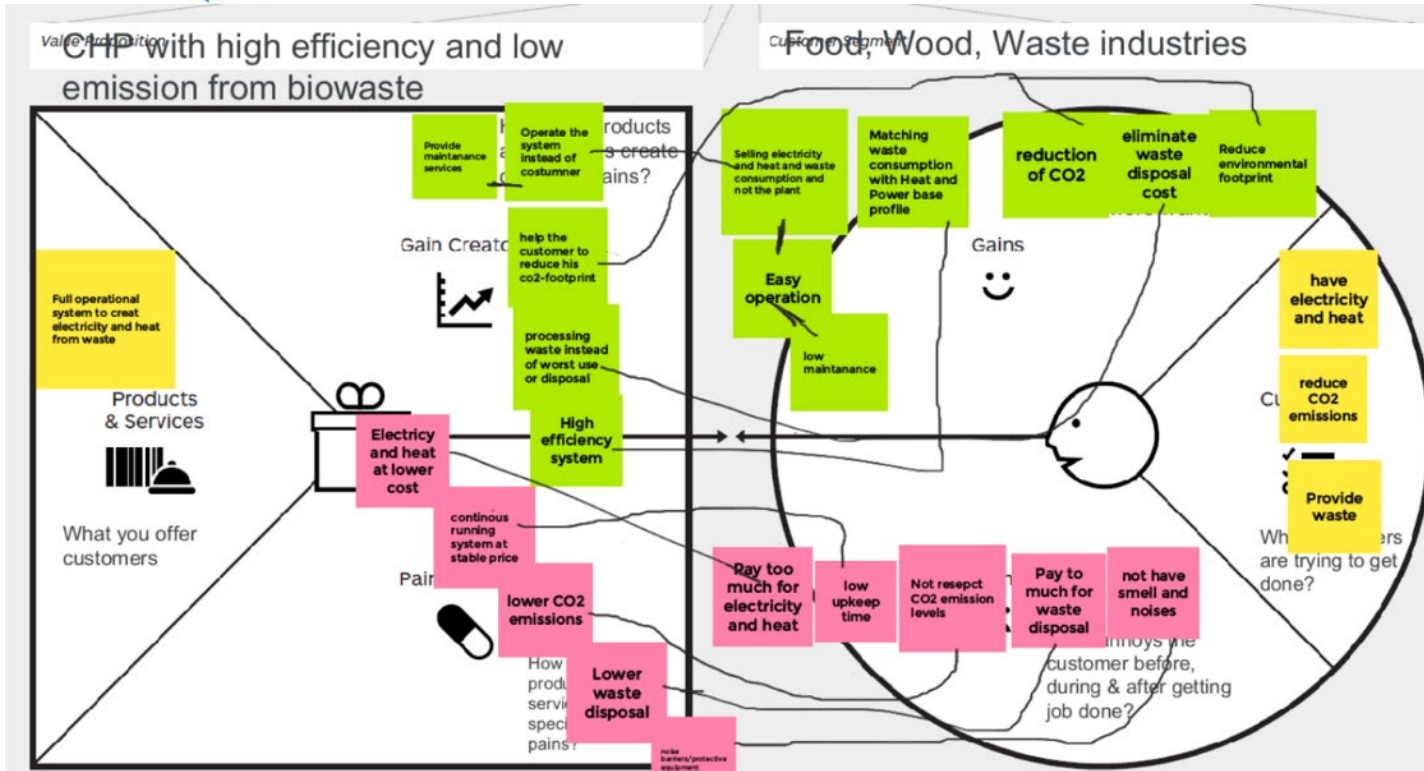




	Unit	Conventional electricity plant	Rough SOFC system	Detailed SOFC System	SOFC in future based on database	Ideal case for BLAZE
Climate change impact	kg CO2 eq	0.77	0.32738	0.33863	0.32901	<b>0.19498</b>
Ecosystem quality	PDF.m2.yr	0.14441	-2.41656	-2.41444	-2.41358	-2.45441
Human health	DALY	1.96E-07	2.57E-07	2.77E-07	2.43E-07	3.49E-07
Water scarcity	m3 world-eq	0.04115	0.01948	-0.00355	0.02266	0.01825
Ozone layer depletion	kg CFC-11 eq	1.83E-07	5.76E-08	6.01E-08	5.81E-08	9.33E-09

	25 kW	50 kW	100 kW	500 kW	1 MW	5 MW	1 MW with 10 years stack lifetime	1 MW with 10 years stack lifetime+future price+2 years maintenance	
<b>No allocation - Do not consider co-generation feature</b>									
CAPEX / 1 kWh electricity	0.390736	0.270921	0.249180	0.216878	0.208223	0.195363	0.104556	<b>0.104556</b>	
OPEX / 1 kWh electricity								0.144339	<b>0.094361</b>
<b>With economic allocation - Consider co-generation feature</b>									
Electricity production									
CAPEX / 1 kWh electricity	0.259105	0.179653	0.165236	0.143816	0.138076	0.129549	0.069333	<b>0.069333</b>	
OPEX / 1 kWh electricity								0.095714	<b>0.062573</b>
Heat production									
CAPEX / 1 kWh heat	0.084629	0.058678	0.053969	0.053969	0.045098	0.042313	0.022646	0.022646	
OPEX / 1 kWh heat								0.031262	0.020437

- ✓ BLAZE pilot plant 0.31 kg CO<sub>2</sub> – eq, 50 % reduction compared with mature electricity generation technology. After reasonable improvement, BLAZE emits 0.19 kg CO<sub>2</sub> – eq. (better heat integration, self-produced **steam**, biofuel instead of **LPG**, renewable electricity, **catalyst** production and lifetime)
- Biomass and maintenance contribute the most in OPEX. Electricity contributes 66% of overall revenues. Economic allocation method is important and necessary to use. BLAZE system has the potential to reach 0.1 Euro/ 1 kWh electricity, 0.04 Euro/ 1 kWh heat (cheaper than the market price), reach BLAZE proposed target. BLAZE shows more competitiveness marketplace when the plant size is big, and it can deliver heat and electricity continuously (CHP).



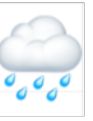
### Strengths

- CHP is energy efficient
- Storage
- Blaze has good Bio CHP characteristics
- Smaller size



### Weaknesses

- Complex plant (leading also to higher CAPEX and O&M costs)
- Limited no. of operational hours leading reliability
- Biomass supply



### Opportunities

- Global energy crisis
- Local autonomy is trendy
- Reduction of CO2 and emissions
- Climate change increasingly actual



### Threats

- Objections of decision-makers
- CAPEX of standard CHP



Business Case Wood Furniture Industry: Heat Demand 5.500 MWh/year, Electricity Demand 9.000 MWh/year  
Sawdust waste-biomass 5.500ton/year 20.000 MWh/year

	CASE 1	CASE 2	CASE 3	CASE 4
Investment	€ 11,135,616.03	€ 8,814,258.58	€ 6,254,416.20	€ 11,135,616.03
Cash Flow (Year 1)	€ 1,919,304.22	€ 1,913,212.58	€ 1,567,033.89	€ 2,074,064.22
LSM cost replacement @y10	€ 7,950,000.00	€ 6,000,000.00	€ 3,900,000.00	€ 7,950,000.00
IRR (Internal Rate of Return)	0.09	0.15	0.19	0.11
NPV - Net Present Value	€ 20,957,466.77	€ 22,072,590.67	€ 18,701,478.17	€ 23,040,878.45



Technology roadmap: Reduce the plant and single equipment costs, Optimize the overall plant cost defining a modular standard size, Cumulate operational manhours for increasing reliability and availability, LSM costs drive the economics (LSM 4.000 €/kWe 5 years lifetime).  
Business Model: ESCO Model seems to be a viable solution for medium scale plants and in general for customers like industries



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*Blaze (@BlazeProject) Twitter / LinkedIn / Facebook*